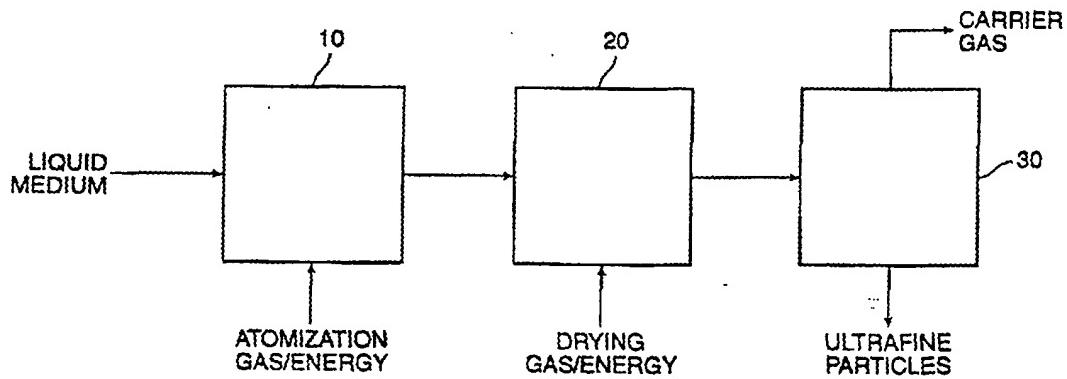




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(54) Title: PROCESSES FOR SPRAY DRYING SOLUTIONS OF HYDROPHOBIC DRUGS WITH HYDROPHILIC EXCIPIENTS AND COMPOSITIONS PREPARED BY SUCH PROCESSES



## (57) Abstract

Methods for preparing dry powders having hydrophobic and hydrophilic components comprise combining solutions or suspensions of the components and spray drying them simultaneously in a spray drier (The Figure). Both the hydrophobic and hydrophilic component are dissolved in a solvent system selected to have adequate solubility of both components. The method provides dry powders having relatively uniform characteristics.

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5                   **PROCESSES FOR SPRAY DRYING SOLUTIONS OF  
HYDROPHOBIC DRUGS WITH HYDROPHILIC EXCIPIENTS  
AND COMPOSITIONS PREPARED BY SUCH PROCESSES**

10                  This application is a continuation-in-part of  
Provisional Application No. 60/034,837, filed on December 31,  
1996, the full disclosure of which is incorporated herein by  
reference.

15                  **BACKGROUND OF THE INVENTION**

1. Field of the Invention

20                  The present invention relates generally to dry  
powder compositions and methods for their preparation and use.  
In particular, the present invention relates to methods for  
spray drying pharmaceutical and other compositions comprising  
a hydrophobic drug or other component and a hydrophilic  
excipient or other component.

25                  Over the years, certain drugs have been sold in  
formulations suitable for oral inhalation (pulmonary delivery)  
to treat various conditions in humans. Such pulmonary drug  
delivery formulations are designed to be inhaled by the  
patient so that the active drug within the dispersion reaches  
the lung. It has been found that certain drugs delivered to  
the lung are readily absorbed through the alveolar region  
directly into blood circulation. Such pulmonary delivery can  
be effective both for systemic delivery and for localized  
30                  delivery to treat diseases of the lungs.

35                  Pulmonary drug delivery can itself be achieved by  
different approaches, including liquid nebulizers, aerosol-  
based metered dose inhalers (MDI's), and dry powder dispersion  
devices. Aerosol-based MDI's are losing favor because they  
rely on the use of chlorofluorocarbons (CFC's), which are  
being banned because of their adverse effect on the ozone  
layer. Dry powder dispersion devices, which do not rely on

CFC aerosol technology, are promising for delivering drugs that may be readily formulated as dry powders.

The ability to deliver pharmaceutical compositions as dry powders, however, is problematic in certain respects.

5      The dosage of many pharmaceutical compositions is often critical, so it is desirable that dry powder delivery systems be able to accurately, precisely, and reliably deliver the intended amount of drug. Moreover, many pharmaceutical compositions are quite expensive. Thus, the ability to  
10     efficiently formulate, process, package, and deliver the dry powders with a minimal loss of drug is critical. With dry powder drug delivery, both the delivered dose efficiency, i.e. the percentage of drug from a unit dose receptacle which is aerosolized and delivered from a delivery device, and the  
15     median particle size distribution, i.e. the deviation from the median size, are critical to the successful delivery of powders to a patient's lungs.

A particularly promising approach for the pulmonary delivery of dry powder drugs utilizes a hand-held device with a hand pump for providing a source of pressurized gas. The pressurized gas is abruptly released through a powder dispersion device, such as a venturi nozzle, and the dispersed powder made available for patient inhalation. While advantageous in many respects, such hand-held devices are problematic in a number of other respects. The particles being delivered are usually less than 5  $\mu\text{m}$  in size, making powder handling and dispersion more difficult than with larger particles. The problems are exacerbated by the relatively small volumes of pressurized gas, which are available using hand-actuated pumps. In particular, venturi dispersion devices are unsuitable for difficult-to-disperse powders when only small volumes of pressurized gas are available with the handpump. Another requirement for hand-held and other powder delivery devices is efficiency. High device efficiency in  
25     delivering the drug to the patient with the optimal size distribution for pulmonary delivery is essential for a commercially viable product.

Spray drying is a conventional chemical processing unit operation used to produce dry particulate solids from a variety of liquid and slurry starting materials. The use of spray drying for the formulation of dry powder pharmaceuticals is known, but has usually been limited to spray drying of hydrophilic drugs in aqueous solutions, usually in combination with hydrophilic excipients. Many drugs, however, are hydrophobic, preventing spray drying in aqueous solutions. While spray drying of hydrophobic materials can often be accomplished using an organic solvent, the use of such non-aqueous solvents generally limits the ability to simultaneously spray dry a hydrophilic excipient.

For these reasons, it would be desirable to provide improved methods for spray drying pharmaceutical and other compositions which comprise both hydrophobic and hydrophilic components, such as hydrophobic drugs and hydrophilic excipients. Such spray drying methods should be compatible with a wide variety of hydrophobic drugs as well as conventional hydrophilic excipients, such as povidone (polyvinylpyrrolidone) and other water soluble polymers, mannitol and other water soluble carbohydrates, and particularly with those excipients which are accepted for use in inhalation formulations, such as lactose and sodium chloride. Such spray drying methods will preferably produce particles having a uniform size distribution, with a mean particle size below 10  $\mu\text{m}$ , preferably below 5  $\mu\text{m}$ , and a standard deviation less than or equal to  $\pm 2 \mu\text{m}$ . Such powders should further exhibit uniform composition from batch to batch so that any tendency for particles of different compositions and/or sizes to separate in the lungs will have a reproducible impact on the therapeutic effect. Additionally, such spray drying methods should provide for dry powders which are physically and chemically stable and which have low levels of any residual organic solvents or other components which might be used in the spray drying process. At least some of the above objectives will be met by the various embodiments of the present invention which are described in detail below.

2. Description of the Background Art

Methods for spray drying hydrophobic and other drugs and components are described in U.S. Patent Nos. 5,000,888; 5,026,550; 4,670,419, 4,540,602; and 4,486,435. Bloch and Speison (1983) *Pharm. Acta Helv* 58:14-22 teaches spray drying of hydrochlorothiazide and chlorthalidone (lipophilic drugs) and a hydrophilic adjuvant (pentaerythritol) in azeotropic solvents of dioxane-water and 2-ethoxyethanol-water. A number of Japanese Patent application Abstracts relate to spray drying of hydrophilic-hydrophobic product combinations, including JP 806766; JP 7242568; JP 7101884; JP 7101883; JP 71018982; JP 7101881; and JP 4036233. Other foreign patent publications relevant to spray drying hydrophilic-hydrophobic product combinations include FR 2594693; DE 2209477; and WO 88/07870.

WO 96/09814 describes spray dried pharmaceutical powders. In particular, Example 7 describes spray drying budesonide and lactose in ethanol where the budesonide is partially soluble and the lactose is insoluble. U.S. Patent Nos. 5,260,306; 4,590,206; GB 2 105 189; and EP 072 046 describe a method for spray drying nedocromil sodium to form small particles preferably in the range from 2 to 15  $\mu\text{m}$  for pulmonary delivery. U.S. Patent No. 5,376,386, describes the preparation of particulate polysaccharide carriers for pulmonary drug delivery, where the carriers comprise particles sized from 5 to 1000  $\mu\text{m}$ . Mumenthaler et al. (1994) *Pharm. Res.* 11:12 describes recombinant human growth hormone and recombinant tissue-type plasminogen activator. WO 95/23613 describes preparing an inhalation powder of DNase by spray drying using laboratory-scale equipment. WO 91/16882 describes a method for spray drying proteins and other drugs in liposome carriers.

The following applications assigned to the assignee of the present application each describe that spray drying may be used to prepare dry powders of biological macromolecules; application serial no. 08/644,681, filed on May 8, 1996, which was a continuation-in-part of application serial no. 08/423,515, filed on April 14, 1995; application serial no.

08/383,475, which was a continuation-in-part of application serial no. 08/207,472, filed on March 7, 1994; application serial no. 08/472,563, filed on April 14, 1995, which was a continuation-in-part of application serial no. 08/417,507, filed on April 4, 1995, now abandoned, which was a continuation of application no. 08/044,358, filed on April 7, 1993, now abandoned; application serial no. 08/232,849, filed on April 25, 1994, which was a continuation of application serial no. 07/953,397, now abandoned. WO 94/07514 claims priority from serial no. 07/953,397. WO 95/24183 claims priority from serial nos. 08/207,472 and 08/383,475.

#### SUMMARY OF THE INVENTION

According to the present invention, methods for spray drying hydrophobic drugs and other materials are provided which overcome at least some of the deficiencies noted above with respect to prior spray drying processes. In particular, the spray drying methods of the present invention permit the simultaneous spray drying of the hydrophobic component with a hydrophilic component, such as a hydrophilic pharmaceutical excipient, under conditions which result in a dry powder comprising mixtures of both the hydrophilic and hydrophobic components. Although the methods of the present invention are particularly useful for forming pharmaceutical compositions where the hydrophobic component is a hydrophobic drug, usually present at from 0.01% to 95% of the powder, and the hydrophilic component is a hydrophilic excipient, usually present at from 99.99% to 5% of the powder, the methods may be applied more broadly to form dry powders comprising a variety of hydrophobic and hydrophilic components at different concentration ranges, including hydrophilic drugs and hydrophobic excipients.

The spray drying methods of the present invention are compatible with many hydrophilic pharmaceutical excipients, particularly including mannitol, povidone, lactose and sodium chloride. Use of the latter two excipients is particularly preferred for powders intended for pulmonary

delivery as they are "generally recognized as safe" (GRAS) for such applications. The methods are also suitable for use with numerous hydrophobic drugs and nutrients, including steroids and their salts, such as budesonide, testosterone,  
5 progesterone, estrogen, flunisolide, triamcinolone, beclomethasone, betamethasone; dexamethasone, fluticasone, methylprednisolone, prednisone, hydrocortisone, and the like; peptides, such as cyclosporin and other water insoluble peptides; retinoids, such as all-cis retinoic acid, 13-trans  
10 retinoic acid, and other vitamin A and beta carotene derivatives; vitamins D, E, and K and water insoluble precursors and derivatives thereof; prostagladins and leukotrienes and their activators and inhibitors including prostacyclin (epoprostanol), prostaglandins E<sub>1</sub> E<sub>2</sub>,  
15 tetrahydrocannabinol; lung surfactant lipids; lipid soluble antioxidants; hydrophobic antibiotics and chemotherapeutic drugs such as amphotericin B, adriamycin, and the like.

The spray drying methods can produce a uniform particle size distribution. For example, the mean particle diameter can be controlled below 10  $\mu\text{m}$ , preferably below 5  $\mu\text{m}$ , with a size distribution (standard deviation) less than  $\pm$  2  $\mu\text{m}$ . The particles of the powders so produced have a minimum batch-to-batch variability in composition, and are physically and chemically stable. The powders have minimum residual  
20 organic solvents to the extent they may have been used in the spray drying process.

In particular, the method of the present invention comprises at least partially dissolving hydrophilic component in an organic solvent or cosolvent system. The hydrophobic component is at least partially dissolved in the same organic solvent or cosolvent system to produce a solution. The organic solvent solution or cosolvent system is then spray dried to form particles comprising a mixture of the hydrophilic and hydrophobic components. The organic solvent will be selected to provide a solubility for the hydrophilic component of at least 1 mg/ml, preferably at least 5 mg/ml, and a solubility for the hydrophobic component of at least 0.01 mg/ml, preferably at least 0.05 mg/ml. Usually, the  
30  
35

hydrophilic component will have a concentration in the organic solvent or cosolvent system solution from 1 mg/ml to 100 mg/ml, preferably from 5 mg/ml to 60 mg/ml, and the hydrophobic component will have a concentration from 5 0.01 mg/ml to 10 mg/ml, preferably from 0.05 mg/ml to 5 mg/ml. Suitable organic solvents or solvent systems are selected to provide such minimum solubility characteristics, but it is preferred if the organic solvent or cosolvent system provides solubilities well in excess of the stated minimums. The use 10 of a nonaqueous solution will be advantageous for spray drying components that are physically or chemically sensitive to either water while in solution or to residual moisture content in the powder. The utilization of a nonaqueous solution will essentially eliminate the exposure of the component to both 15 water during spray drying and residual moisture in the powder, thereby avoiding triggering the component's sensitivity to water. A presently preferred cosolvent system comprises water:ethanol at a weight ratio in the range from 80:20 to 20:80, usually from 40:60 to 60:40, preferably 50:50. The utilization of a water:ethanol system is preferred for any 20 hydrophobic component and hydrophilic component combination which has adequate solubility and stability in this solvent system, due to the low worker exposure toxicological hazard posed by this solvent system, and because of the lack of 25 toxicity of any residual solvent in the powder after spray drying is complete.

Powders prepared by the above method will be collected from the spray drier in a conventional manner for 30 subsequent use. For use as pharmaceuticals and other purposes, it will frequently be desirable to disrupt any agglomerates which may have formed by screening or other conventional techniques. For pharmaceutical uses, the dry powder formulations will usually be measured into a single dose, and the single dose sealed into a package. Such 35 packages are particularly useful for dispersion in dry powder inhalers, as described in detail below. Alternatively, the powders may be packaged in multiple-dose containers.

The present invention further comprises dry powder compositions produced according to the methods described above, as well as unit dose and multidose packages of such dried powder compositions containing a therapeutically effective amount of the dry powder.

The present invention further provides methods for aerosolizing a dry powder composition comprising the steps of providing an amount of dry powder composition produced by any of the methods described above and subsequently dispersing the dry powder composition into a flowing gas stream.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a block diagram illustrating a spray drying system suitable for performing the methods of the present invention.

#### DETAILED DESCRIPTION OF THE SPECIFIC EMBODIMENTS

The present invention relates to methods for preparing compositions comprising ultrafine dry powders having both hydrophobic and hydrophilic components. The methods are particularly suitable for producing ultrafine pharmaceutical dry powders where the hydrophobic component is a hydrophobic drug and the hydrophilic component is a hydrophilic excipient. The present invention, however, may find use for preparing a variety of other compositions including pharmaceutical compositions having hydrophilic drugs and hydrophobic excipients and compositions intended for non-pharmaceutical applications. The methods rely on spray drying liquid media in which the components are solubilized or suspended. In particular, an organic solvent or cosolvent system is selected which can solubilize both the hydrophobic and the hydrophilic component.

The term "hydrophobic component" refers to materials which are insoluble or sparingly or poorly soluble in water. As used herein, such compositions will have a solubility below 5 mg/ml, usually below 1 mg/ml. Exemplary hydrophobic drugs include certain steroids, such as budesonide, testosterone, progesterone, estrogen, flunisolide, triamcinolone,

beclomethasone, betamethasone; dexamethasone, fluticasone, methylprednisolone, prednisone, hydrocortisone, and the like; certain peptides, such as cyclosporin cyclic peptide, retinoids, such as all-cis retinoic acid, 13-trans retinoic acid, and other vitamin A and beta carotene derivatives; vitamins D, E, and K and water insoluble precursors and derivatives thereof; prostagladins and leukotrienes and their activators and inhibitors including prostacyclin (epoprostanol), prostaglandins E<sub>1</sub> E<sub>2</sub>, tetrahydrocannabinol; lung surfactant lipids; lipid soluble antioxidants; hydrophobic antibiotics and chemotherapeutic drugs such as amphotericin B and adriamycin and the like.

By "hydrophilic component," it is meant that the component is highly soluble in water and frequently capable of swelling and formation of reversible gels. Typical aqueous solubilities of hydrophilic components will be greater than 5 mg/ml, usually greater than 50 mg/ml, and often much higher. In addition to their hydrophilic nature, the pharmaceutical excipients will generally be selected to provide stability, dispersibility, consistency and/or bulking characteristics to enhance the uniform pulmonary delivery of the dried powder composition to a patient. For pulmonary delivery, the excipients must be capable of being taken into the lungs with no significant adverse toxicological effects on the lungs. Exemplary hydrophilic excipients include carbohydrates and other materials selected from the group consisting of lactose, mannitol, povidone, sodium chloride, water soluble polymers, and the like. Particularly preferred are lactose and sodium chloride which are generally accepted for pulmonary delivery in dry powder formulations.

The phrase "ultrafine dry powder" means a powder composition comprising a plurality of discrete, dry particles having the characteristics set forth below. In particular, the dry particles will have an average particle size below 10  $\mu\text{m}$ , usually below 5  $\mu\text{m}$ , preferably being in the range from 0.4 to 5  $\mu\text{m}$ , more preferably from 0.4 to 4  $\mu\text{m}$ . The average particle size of the powder will be measured as mass median diameter (MMD) by conventional techniques. A particular

5 powder sizing technique uses a centrifugal sedimentary particle size analyzer (Horiba Capa 700). The powders will be capable of being readily dispersed in an inhalation device and subsequently inhaled by a patient so that the particles are able to penetrate into the alveolar regions of the lungs.

10 Of particular importance to the present invention, the ultrafine dry particle compositions produced by the method will have particle size distributions which enable them to target the alveolar region of the lung for pulmonary delivery of locally acting steroids, systemically acting proteins, and other biologically active materials that can be administered to or through the lungs. Such compositions advantageously may be incorporated into unit dosage and other forms without further size classification. Usually, the ultrafine dry  
15 powders will have a size distribution where at least 90% of the powder by weight will comprise particles having an average size in the range from 0.1  $\mu\text{m}$  to 7  $\mu\text{m}$ , with preferably at least 85% being in the range from 0.4  $\mu\text{m}$  to 5  $\mu\text{m}$ . Additionally, it is desirable that the particle size  
20 distribution avoid having an excess amount of particles with very small average diameters, i.e., below 0.4  $\mu\text{m}$ .

25 The term "dry" means that the particles of the powder have a moisture content such that the powder is physically and chemically stable in storage at room temperature and is readily dispersible in an inhalation device to form an aerosol. Usually, the moisture and residual solvent content of the particles is below 10% by weight, usually being below 5% by weight, preferably being below 3% by weight, or lower. The moisture and residual solvent content  
30 will usually be controlled by the drying conditions, as described in more detail below. The term "dry" further means that the particles of the powder have a moisture and residual solvent content such that the powder is readily dispersible in an inhalation device to form an aerosol. In some cases, however, non-aqueous medium may be used for dispersing the components, in which case the aqueous content may approach zero.

The term "therapeutically effective amount" is the amount present in the composition that is needed to provide the desired level of hydrophobic drug in the subject to be treated to give the anticipated physiological response. This 5 amount is determined for each drug on a case-by-case basis. The term "physiologically effective amount" is that amount delivered to a subject to give the desired palliative or curative effect. This amount is specific for each drug and its ultimate approval dosage level.

10 The therapeutically effective amount of hydrophobic drug will vary in the composition depending on the biological activity of the drug employed and the amount needed in a unit dosage form. Because the subject powders are dispersible, it is highly preferred that they be manufactured in a unit dosage 15 form in a manner that allows for ready manipulation by the formulator and by the consumer. This generally means that a unit dosage will be between about 0.5 mg and 15 mg of total material in the dry powder composition, preferably between about 1 mg and 10 mg. Generally, the amount of hydrophobic 20 drug in the composition will vary from about 0.01% w/w to about 95% w/w. Most preferably the composition will be about 0.05% w/w to about 25% w/w drug.

Referring now to Fig. 1, processes according to the present invention for preparing dispersible dry powders of 25 hydrophobic and hydrophilic components comprise an atomization operation 10 which produces droplets of a liquid medium which are dried in a drying operation 20. Drying of the liquid droplets results in formation of the discrete particles which form the dry powder compositions which are then collected in a 30 separation operation 30. Each of these unit operations will be described in greater detail below.

The atomization process 10 may utilize any one of several conventional forms of atomizers. The atomization process increases the surface area of the starting liquid. 35 Due to atomization there is an increase in the surface energy of the liquid, the magnitude of which is directly proportional to the surface area increase. The source of this energy increase depends on the type of atomizer used. Any atomizer

(centrifugal, sonic, pressure, two fluid) capable of producing droplets with a mass median diameter of less than about 20  $\mu\text{m}$  could be used. Preferred for the present invention is the use of two fluid atomizers where the liquid medium is delivered through a nozzle concurrently with a high pressure gas stream. Particularly preferred is the use of two-fluid atomization nozzles as described in copending application serial no. 08/644,681, which is capable of producing droplets having a median diameter less than 20  $\mu\text{m}$ .

The atomization gas will usually be nitrogen which has been filtered or otherwise cleaned to remove particulates and other contaminants. Alternatively, other gases, such as air may be used. The atomization gas will be pressurized for delivery through the atomization nozzle, typically to a pressure above 5 psig, preferably being above 10 psig. Although flow of the atomization gas is generally limited to sonic velocity, the higher delivery pressures result in an increased atomization gas density. Such increased gas density has been found to reduce the droplet size formed in the atomization operation. Smaller droplet sizes, in turn, result in smaller particle sizes. The atomization conditions, including atomization gas flow rate, atomization gas pressure, liquid flow rate, and the like, will be controlled to produce liquid droplets having an average diameter below 20  $\mu\text{m}$  as measured by phase doppler velocimetry.

The drying operation 20 will be performed next to evaporate liquid from the droplets produced by the atomization operation 10. Usually, the drying will require introducing energy to the droplets, typically by mixing the droplets with a heated gas which causes evaporation of the water or other liquid medium. Preferably, the heated gas stream will flow concurrently with the atomized liquid, but it would also be possible to employ counter-current flow, cross-current flow, or other flow patterns.

The drying rate may be controlled based on a number of variables, including the droplet size distribution, the inlet temperature of the gas stream, the outlet temperature of the gas stream, the inlet temperature of the liquid droplets,

and the manner in which the atomized spray and hot drying gas are mixed. Preferably, the drying gas stream will have an inlet temperature of at least 70°C. The outlet temperature will usually be at least about 40°C. The drying gas will usually be air or nitrogen which has been filtered or otherwise treated to remove particulates and other contaminants. The gas will be moved through the system using conventional blowers or compressors.

The separation operation 30 will be selected in order to achieve very high efficiency collection of the ultrafine particles produced by the drying operation 20. Conventional separation operations may be used, although in some cases they should be modified in order to assure collection of sub-micron particles. In an exemplary embodiment, separation is achieved using a filter medium such as a membrane medium (bag filter), a sintered metal fiber filter, or the like. Alternatively, and often preferably, separation may be achieved using cyclone separators, although it is usually desirable to provide for high energy separation in order to assure the efficient collection of sub-micron particles. The separation operation should achieve collection of at least 80% of all particles above 1  $\mu\text{m}$  in average particle size, preferably being above 85%, more preferably being above 90%, and even more preferably being above 95%, in collection efficiency.

In some cases, a cyclone separator can be used to separate very fine particles, e.g. 0.1  $\mu\text{m}$ , from the final collected particles. The cyclone operating parameters can be selected to provide an approximate cutoff where particles above about 0.1  $\mu\text{m}$  are collected while particles below 0.1  $\mu\text{m}$  are carried over in the overhead exhaust. The presence of particles below 0.1  $\mu\text{m}$  in the pulmonary powder is undesirable since they will generally not deposit in the alveolar regions of the lungs, but instead will be exhaled.

The present invention relies on proper selection of the liquid medium or media for solubilizing the hydrophobic drug or other component and hydrophilic excipient or other component. An organic solvent or cosolvent is selected in

which both the hydrophobic drug or other component and the hydrophilic excipient or other component may be dissolved. Neither the drug nor excipient need be highly soluble in the solvent, since both components will typically be present in the solvent at relatively low concentrations, usually below 10% w/v, more usually below 5% w/v. The solvent must further be selected to leave minimum residual solvent in the spray dried product. The particular organic solvent or cosolvent selected will depend on the nature of the hydrophobic drug and the hydrophilic excipient. Suitable organic solvents or solvent systems may include an alcohol, ketone, hydrocarbon, polar aprotic solvent, or the like, and mixtures and aqueous solutions thereof. The use of a nonaqueous solution will be advantageous for spray drying components that are physically or chemically sensitive to either water while in solution or to residual moisture content in the powder. The utilization of a nonaqueous solution will essentially eliminate the exposure of the component to both water during spray drying and residual moisture in the powder, thereby avoiding triggering the component's sensitivity to water. Exemplary combinations of drug, excipient, and solvent are set forth in Table 1 below.

TABLE I

DRUG (Solubility in Solvent)	EXCIPIENT (Solubility in Solvent)	SOLVENT
Budesonide (good solubility)	Povidone (highly soluble)	Methanol
Budesonide (adequate solubility)	Povidone (good solubility)	Ethanol
Budesonide (adequate solubility)	Mannitol (adequate solubility)	Acetone (50%)/ Water (50%) (by volume)
Budesonide (good solubility)	Lactose (adequate solubility)	DMSO (33%)/ Acetone (67%) (by volume)
Budesonide (adequate solubility)	Lactose and/or Sodium Chloride (adequate solubility)	Ethanol (50%)/ Water (50%) (by volume)

Each of these formulations has been spray dried and tested as described in further detail in the Experimental section hereinafter. It should be noted that for many pharmaceutical compositions, it will be desirable to provide the excipient at significantly higher concentrations than the drug. Thus, when choosing a common solvent system it may be necessary to choose solvents which provide for greater solubility for the excipient than for the drug. A presently preferred cosolvent comprises water:ethanol in the ratios set forth above. The utilization of an ethanol/water system is preferred for any hydrophobic component and hydrophilic component combination which has adequate solubility and stability in this solvent system, due to the low worker exposure toxicological hazard posed by this solvent system, and because of the lack of toxicity of any residual solvent in the powder after spray drying is complete.

This spray drying method, which employs a common solubilizing solvent system, is advantageous in that both the hydrophobic drug or other component and the hydrophilic excipient or other component will be fully dissolved, enhancing product uniformity after spray drying. The full dissolution of the component is desirable since it greatly reduces the likelihood that the components will separate to any significant extent during storage, delivery to the spray drier, passage through the atomization nozzle, or during the spray drying operation.

Once the dry powders have been prepared, they may be packaged in conventional ways. For pulmonary pharmaceutical applications, unit dosage forms may comprise a unit dosage receptacle containing a dry powder. The powder is placed within a suitable dosage receptacle in an amount sufficient to provide a subject with drug for a unit dosage treatment. The dosage receptacle is one that fits within a suitable inhalation device to allow for the aerosolization of the dry powder composition by dispersion into a gas stream to form an aerosol and then capturing the aerosol so produced in a chamber having a mouthpiece attached for subsequent inhalation by a subject in need of treatment. Such a dosage receptacle

includes any container enclosing the composition known in the art such as gelatin or plastic capsules with a removable portion that allows a stream of gas (e.g., air) to be directed into the container to disperse the dry powder composition.

5 Such containers are exemplified by those shown in U.S. Patents 4,227,522 issued October 14, 1980; 4,192,309 issued March 11, 1980; and 4,105,027 issued August 8, 1978. Suitable containers also include those used in conjunction with Glaxo's Ventolin Rotohaler® brand powder inhaler or Fison's Spinhaler®  
10 brand powder inhaler. Another suitable unit-dose container which provides a superior moisture barrier is formed from an aluminum foil plastic laminate. The pharmaceutical-based powder is filled by weight or by volume into the depression in the formable foil and hermetically sealed with a covering  
15 foil-plastic laminate. Such a container for use with a powder inhalation device is described in U.S. patent 4,778,054 and is used with Glaxo's Diskhaler® (U.S. Patents 4,627,432; 4,811,731; and 5,035,237). Preferred dry powder inhalers are those described in U.S. Patent application serial nos.  
20 08/309,691 and 08/487,184, assigned to the assignee of the present invention. The latter application has been published as WO 96/09085.

The following examples are offered by way of illustration, not by way of limitation.

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#### EXPERIMENTAL

The following materials were used:

Budesonide (micronized to a median particle size of 1-2  $\mu\text{m}$ ;  
30 Steraloids)

Lactose monohydrate (NF grade; Foremost Ingredient Group)

Povidone (PVP K-15; ISP Technologies)

Mannitol (USP grade; Mallinckrodt)

Sodium Chloride (reagent grade from VWR and USP grade from EM  
35 Industries)

Deionized water

Ethanol, 200 proof (USP/NF; Spectrum Chemical Mfg. Corp.)

Acetone (for histology; EM Industries)

Methanol (HPLC grade; EM Industries)

Dimethyl sulfoxide (DMSO; Photex reagent grade; J.T. Baker)

All batches were spray dried on Buchi 190 Mini Spray Dryers, with nozzles and cyclones that were designed to generate and catch very fine particles. Since these formulations utilized organic solvents, a Buchi 190 Mini Spray Dryer was used that was modified so that it was supplied with nitrogen as the gas source and equipped with an oxygen sensor and other safety equipment to minimize the possibility of explosion. The solution feed rate was 5 ml/minute, inlet temperature was adjusted to obtain the outlet temperature noted in each example, the top of the cyclone in some runs was jacketed and cooled to a temperature of about 30°C, the drying nitrogen flow rate was about 18 SCFM, and the atomizing nitrogen was supplied at 0.5 to 1.5 SCFM. The powders were further dried in the collector for 5-15 minutes (most often for 5 minutes) by maintaining approximately the outlet temperature and air volume after the feeding of the liquid formulation was completed.

Particle size was determined with a Horiba Particle Size Analyzer, model CAPA 700. Median particle size refers to the volume based particle size distribution of the prepared bulk powders determined via centrifugal sedimentation as follows. A sample of the powder was suspended in an appropriate liquid medium (one that minimizes solubilizing the particle), sonicated to break up the agglomerates, and then centrifuged. The median particle size was determined by measuring the sedimentation rate during centrifugation. This method provides the median size of the "primary" particle, that is, the size of the particles produced by the manufacturing process, plus potential modification during sample preparation. Because these formulations are composed of both water soluble and water insoluble materials, it is likely that the suspension step during sample preparation does to some extent solubilize part of the particle, and thereby modify the particle size that is determined. Therefore, the resultant particle sizes should be viewed as estimated values, rather than absolute values.

Moisture content was determined by the Karl-Fischer Reagent titrimetric method.

Delivered dose efficiency refers to a measure of the percentage of powder which is drawn out of a blister package and which exits the mouthpiece of an inhaler device as described in U.S. Patent Application Serial No. 08/487,184.

Delivered dose efficiency is a measure of efficiency for the powder package/device combination. The test was performed by connecting a vacuum system to the device mouthpiece. The vacuum system was set to be similar to a human inhalation with regard to volume and flow rate (1.2 liters total at 30 liters/minute). A blister package containing 0.5 to 10 mg of the formulation to be evaluated (2 to 5 mg of powder was used for the following examples) was loaded into a device which was held in a testing fixture. The device was pumped and fired, and the vacuum "inhalation" was switched on. The aerosol cloud was thus drawn out of the device chamber by the vacuum, and the powder was collected on a filter placed between the mouthpiece and the vacuum source. The weight of the powder collected on the filter was determined. Delivered dose efficiency was calculated by multiplying this weight by one hundred and dividing by the fill weight in the blister. A higher number was a better result than a lower number.

Solubilizing both budesonide and excipient in an organic solvent system

Manufacturing procedure:

The indicated amounts of the budesonide and the excipient(s) were mixed with the indicated amount of the liquid medium until all of the solids were completely dissolved to form a solution. If necessary the solution was sonicated to fully dissolve the solids. For the examples utilizing 50:50 ethanol:water as the solvent system, the indicated amount of budesonide was dissolved in the indicated amount of ethanol with mixing, the indicated amount of excipient(s) was dissolved in the indicated amount of water with mixing, and then the two solutions were mixed together, resulting in a single solution containing all of the

components. The solution was spray dried, and the resulting powder passed through a 35 mesh screen. This last step may not always be required, but it has been found that passing the powder through a screen will often decrease the delivered dose 5 efficiency variability.

Table 2 shows the spray drier atomization air pressure and outlet air temperature, the quantitative composition, a description of the particle morphology, the moisture content where water was a component in the liquid 10 medium, particle size, and delivered dose efficiency for each powder. Where the powders were passed through a 35 mesh screen, the delivered dose efficiency results are preceded by the word "screened." It is noteworthy that the use of a 1:2 DMSO/acetone liquid medium yielded low delivered dose 15 efficiency results as did the formulation where sodium chloride was the sole excipient.

**TABLE 2**  
**Solubilizing both budesonide and excipient in an organic solvent system**

Batch No., Formula No. (Spray Drier Atomization Air Pressure/Outlet Air Temperature)	Quantitative Composition	Particle Morphology	Moisture Content	Particle Size ( $\mu\text{m}$ )	Delivered Dose Efficiency	
					5	10
329-20 B-51 (15PSI/57°C)	Budesonide Mannitol 1:1 Acetone:DI water	75 mg 1425 mg 50 ml	Slightly dimpled spheres	0.49%	2.31	47.2% (RSD=12)
329-39 B-51 (15PSI/57°C)	Budesonide Mannitol 1:1 Acetone:DI water	350 mg 6650 mg 233 ml		0.51%	2.35	Screened: retest: retest:
329-39 B-51 (15PSI/57°C)	Budesonide Mannitol 1:1 Acetone:DI water	350 mg 6650 mg 233 ml		0.50%	1.93	55.4% (RSD=7) 51.2% (RSD=10) 52.2% (RSD=13)
329-22 B-52 (20PSI/66°C)	Budesonide PVP K-15 Ethanol	75 mg 1425 mg 50 ml	No water in formula	3.59	47.9% (RSD=11)	
329-23 B-52 (15PSI/76°C)	Budesonide PVP K-15 Ethanol	75 mg 1425 mg 50 ml	No water in formula	3.39	52.1% (RSD=9)	
329-46 B-52 (15PSI/76°C)	Budesonide PVP K-15 Ethanol	75 mg 1425 mg 50 ml	Dimpled spheres	1.09	44.8% (RSD=20)	
329-62 B-52 (15PSI/76°C)	Budesonide PVP K-15 Ethanol	75 mg 1425 mg 50 ml	Dimpled spheres	1.09	50.3% (RSD=22)	
329-78-S B-52 (15PSI/76°C)	Budesonide PVP K-15 Ethanol	350 mg 6650 mg 233 ml	No water in formula	2.51	49.8% (RSD=28) 60.5 (RSD=7)	
329-25 B-53 (20PSI/66°C)	Budesonide PVP K-15 Methanol	350 mg 1425 mg 50 ml	No water in formula	2.26	43.7% (RSD=13)	
329-30 B-5 (15PSI/68°C)	Budesonide Lactose 1:2 DMSO:acetone	75 mg 1425 mg 75 ml	No water in formula	4.15	44.8% (RSD=9)	
329-31 B-5 (10PSI/73°C)	Budesonide Lactose 1:2 DMSO:acetone	75 mg 1425 mg 75 ml	Plates	Not available	46.3% (RSD=14) 35.6% (RSD=8)	
						13.6% (RSD=31)
						6.3% (RSD=45)

Table 2 (Continued)

Batch No., Formula No., (Spray Drier Atomization Air Pressure/Outlet Air Temperature)	Quantitative Composition	Particle morphology	Moisture Content	Particle Size ( $\mu\text{m}$ )	Delivered Dose Efficiency
633-64-S B-125 (105PSI/77°)	Budesonide Lactose Ethanol DI water	960 mg 5040 mg 150 ml 150 ml	Smooth spheres	0.9%	1.88 Screened: 56.9% (RSD=8)
633-25-S B-120 (105PSI/77°)	Budesonide Lactose Sodium Chloride Ethanol DI water	960 mg 2520 mg 2520 mg 150 ml 150 ml	Highly dimpled spheres	0. 9%	1.84 Screened: 60.1% (RSD=6)
633-77-S B-127 (105PSI/77°)	Budesonide Sodium Chloride Ethanol DI water	960mg 5040 mg 150 ml 150 ml	Cubes and agglomerates of cubes	0.3%	1.12 Screened: 16.2% (RSD=19)

Although the foregoing invention has been described in some detail by way of illustration and example, for purposes of clarity of understanding, it will be obvious that certain changes and modifications may be practiced within the scope of the appended claims.

WHAT IS CLAIMED IS:

1           1. A method for preparing a dry powder  
2 composition, said method comprising:  
3           at least partially dissolving a hydrophilic  
4 component in an organic solvent or cosolvent system;  
5           at least partially dissolving a hydrophobic  
6 component in the same organic solvent or cosolvent system to  
7 produce an organic solution; and  
8           spray drying the organic solution, to form particles  
9 comprising a mixture of the hydrophilic and hydrophobic  
10 components.

1           2. A method as in claim 1, wherein the hydrophilic  
2 component has a solubility of at least 1 mg/ml in the organic  
3 solvent or cosolvent system and the hydrophobic component has  
4 a solubility of at least 0.01 mg/ml in the organic solvent or  
5 cosolvent system.

1           3. A method as in claim 2, wherein the hydrophilic  
2 component has a concentration in the range from 1 mg/ml to  
3 100 mg/ml and the hydrophobic component has a concentration in  
4 the range from 0.01 mg/ml to 10 mg/ml.

1           4. A method as in claim 1, wherein the solvent  
2 comprises an alcohol, ketone, hydrocarbon or polar aprotic  
3 solvent, and mixtures and aqueous solutions thereof.

1           5. A method as in claim 1, wherein the solvent  
2 comprises ethanol:water at 80:20 to 20:80 by weight.

1           6. A method as in claim 1, wherein the hydrophobic  
2 component comprises a hydrophobic drug.

1           7. A method as in claim 1, wherein the hydrophobic  
2 drug is a steroid selected from the group consisting of  
3 budesonide, testosterone, progesterone, estrogen, flunisolide,  
4 triamcinolone, beclomethasone, betamethasone; dexamethasone,  
5 fluticasone, methylprednisolone, prednisone, hydrocortisone.

1           8. A method as in claim 1, wherein the hydrophobic  
2 drug comprises a peptide, a retinoid, vitamin D, vitamin E,  
3 vitamin K, precursors and derivatives of these vitamins, a  
4 prostaglandin, a leukotriene, tetrahydrocannabinol, lung  
5 surfactant lipid, an antioxidant, a hydrophobic antibiotic, or  
6 a chemotherapeutic drug.

1           9. A method as in claim 1, wherein the hydrophilic  
2 component comprises an excipient for the hydrophobic drug.

1           10. A method as in claim 9, wherein the hydrophilic  
2 excipient comprises a material selected from the group  
3 consisting of lactose, mannitol, povidone, sodium chloride,  
4 and mixtures thereof.

1           11. A method as in claim 1, further comprising  
2 screening the spray dried particles to disrupt agglomerates.

1           12. A method as in any one of claims 1 to 11,  
2 further comprising:

3           measuring a single dosage of the dry powder; and  
4 sealing the single dosage in a package.

1           13. A dry powder composition prepared according to  
2 any of claims 1 to 11.

1           14. A unit dose of a dry powder composition  
2 comprising a unit dose receptacle having a therapeutically  
3 effective amount of a dry powder composition according to any  
4 one of claims 1 to 11.

1           15. A method for aerosolizing a dry powder  
2 composition said method comprising:

3           providing an amount of a dry powder composition  
4 according to any of claims 1 to 11; and

5           dispersing the dry powder composition into a flowing  
6 gas stream.

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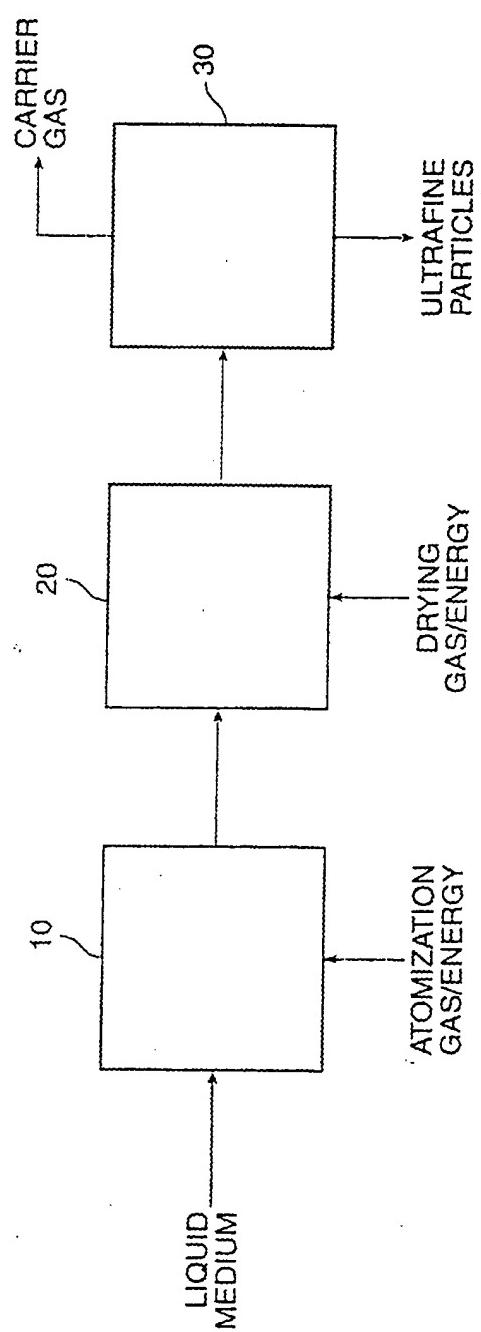


FIG. 1

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US97/23904

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) : A61L 9/04, 9/14  
US CL : 424/45, 46, 434, 435

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 424/45, 46, 434, 435

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 4,590,206 A (FORRESTER ET AL) 20 May 1986, column 4, lines 42-67; column 6, lines 45-59; column 7, lines 62-68; column 8, lines 7-14.	1-11
Y	US 4,540,602 A (MOTOYAMA ET AL) 10 September 1985, column 4, lines 33-43; column 6, lines 38-42; column 7, lines 48-66; column 8, lines 40-45; column 9, lines 6-10, 34-42; column 12, lines 13-17.	1-11
Y	US 5,510,118 A (BOSCH ET AL) 23 April 1996, column 3, lines 65-68; column 4, lines 1-27, 54-68; column 5, lines 1-18, 52-68; column 7, lines 50-62.	1-11

Further documents are listed in the continuation of Box C.  See patent family annex.

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12 MARCH 1998

06 MAY 1998

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Examination No. 17021 200 2220

Patent No. 17021 200 1998

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US97/23904

## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5,376,386 A (GANDERTON ET AL) 27 December 1994, column 2, lines 3-11, 59-62; column 4, lines 8-36.	12-15

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